

SELENIUM TREATMENT ARCH-EASTERN, BIRCH MINE

WEST VIRGINIA MINE DRAINAGE TASK FORCE SYMPOSIUM

March 26, 2013

Conestoga-Rovers & Associates
Arch Coal, Inc.

Conestoga-Rovers & Associates (CRA)

- Al Meek

Arch Coal, Inc.

- Keith Odell

Bratton Farm

- Ben Faulkner

Arch-Eastern, Birch Mine

- In March of 2011 a Consent Decree was entered by WVDEP requiring corrective action to comply with Selenium standard (i.e., 4.7 $\mu\text{g}/\text{l}$ (average) and 8.2 $\mu\text{g}/\text{l}$ (maximum)) at 10 discharge points on the Knight Ink surface mine.
- A corrective action plan developed by Arch and CRA to establish the following:
- **Establish design criteria for treatment of waters associated with discharge points identified in the Consent Decree**
 - **Determine applicability of new and existing selenium treatment technologies**
 - **Complete alternatives analysis of selenium treatment system options.**
 - **Select Treatment Alternative**
 - **Design and construct system**
 - **Initial compliance by August 2012**

Knight Ink Permit S-2019-88



Hydrologic Modeling

- ❖ Consisted of Three Separate Models
 - Surface Runoff
 - Infiltration/Evapotranspiration
 - Pit Floor (Seepage flow)
- ❖ Utilized the EPA developed Storm Water Management Model (PCSWMM)
- ❖ Conducted on-site flow monitoring to calibrate model.
- ❖ Utilized 2010 rainfall data and inserted a 10 yr, 24 hour event.

Modeling Summary by Discharge

| Discharge I.D. | Average runoff (gpm) | Average seep flow (gpm) | Average total flow (gpm) | 10 yr 24 hr storm | | |
|-------------------|-------------------------|----------------------------|-----------------------------|--------------------|-----------------------|-------------------|
| | | | | Peak runoff gpm | Peak seep flow gpm | Total Peak gpm |
| 001 | 77.5 | 86.8 | 164.3 | 5462.0 | 1041.5 | 6503.5 |
| 002 | 88.1 | 72.7 | 160.8 | 6810.7 | 167.6 | 6978.3 |
| 005 | 41.6 | 67.1 | 108.8 | 3602.7 | 225.5 | 3828.2 |
| 006 | 13.4 | 192.4 | 205.8 | 1032.9 | 429.3 | 1462.2 |
| 007 | 31.1 | 97.4 | 128.5 | 3582.1 | 472.9 | 4055.0 |
| 014 | 14.0 | 26.6 | 40.6 | 1057.3 | 102.4 | 1159.7 |
| 021 | 22.7 | 68.4 | 91.0 | 1525.4 | 168.9 | 1694.3 |
| 031 | 22.6 | 77.7 | 100.3 | 1281.1 | 894.7 | 2175.8 |
| 034** | | | | | | |
| 036 | 19.3 | 23.6 | 42.9 | 719.6 | 239.5 | 959.2 |
| Totals | 330.3 | 712.7 | 1,043.0 | 25,073.9 | 3,742.4 | 28,816.3 |

** Discharges into 001, flow included in 001

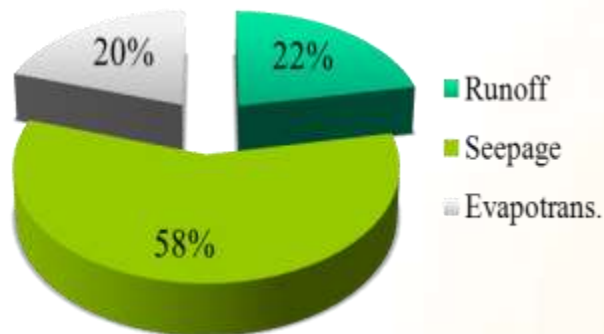
Modeling Summary of Contributing Precipitation

| Rainfall (2010) | Runoff | Seepage | Evapotrans. |
|-----------------|-------------|------------|-------------|
| Total inches | Inches (%) | Inches (%) | Inches (%) |
| 45.87 | 10.10 (22%) | 26.47(58%) | 9.30 (20%) |

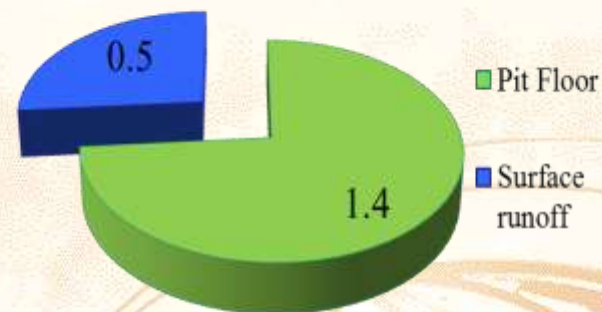
| | Surface Runoff | Pit Floor | Total |
|--------------------------|----------------|-----------|-------|
| Average Gal/min./acre | 0.5 | 1.4 | 1.9 |

Modeling Summary of Contributing Precipitation

Rainfall (2010) – 45.37 inches



Average – 1.9 Gal/min./acre



Determining Design Se Concentrations

From 2010 DMR Data

| Discharge | Average Se Conc. | 95th Percentile Se Conc. | Maximum. Se Conc. |
|------------------|-------------------------|---------------------------------|--------------------------|
| I.D. | µg/l | µg/l | µg/l |
| 001 | 4.59 | 11.13 | 17.50 |
| 002 | 8.38 | 20.03 | 34.90 |
| 005 | 6.97 | 10.40 | 11.60 |
| 006 | 2.10 | 5.95 | 15.10 |
| 007 | 6.21 | 13.34 | 20.50 |
| 014 | 2.47 | 6.80 | 9.00 |
| 021 | 9.66 | 16.34 | 32.90 |
| 031 | 6.72 | 15.94 | 21.00 |
| 034 | 3.82 | 9.50 | 10.60 |
| 036 | 13.25 | 20.45 | 21.20 |

Treatment Design Basis

Basis-- 2010 rainfall Modeled (W. 10yr-24hr) and DMR Selenium Conc.

| Discharge ID. | Average Flow gpm | Average Surface Runoff gpm | Average Seepage Flow gpm | Selenium (2010) Design Conc. µg/l** |
|----------------|---------------------|----------------------------------|--------------------------------|---|
| 001 | 164.29 | 77.5 | 86.8 | 11.1 |
| 002 | 160.82 | 88.1 | 72.7 | 20 |
| 005 | 108.79 | 41.6 | 67.1 | 10.4 |
| 007 | 128.48 | 31.1 | 97.4 | 13.3 |
| 021 | 91.03 | 22.7 | 68.4 | 16.3 |
| 031 | 100.31 | 22.6 | 77.7 | 15.9 |
| 036 | 42.88 | 19.3 | 23.6 | 20.5 |
| Totals | 796.59 | 302.88 | 493.71 | |
| Weight Average | | | | 14.88 |

** 95 th Perentile Se concentrations

Treatment Design Considerations, Centralized vs. Independent

- ❖ Property access, permitting time requirements and jurisdictional wetlands immediately downstream of discharges, dictated that a **centralized treatment approach** be employed.
- ❖ Centralized Collection and Transfer System
 - Water level in ponds will be kept low via level controlled pump.
 - Pumps will deliver water to a centralized location for treatment
- ❖ Benefits of Centralized Collection and Treatment
 - Flow equalization is achieved in existing ponds
 - Treatment system can be constructed in most favorable location
 - Combining of flow allows for a lower Se. design concentration i.e., 95th percentile vs. max concentration

Centralized Collection and Transfer System



Centralized Collection and Transfer System (20,000 ft. Pipeline Transfer System)



Centralized Collection and Transfer System

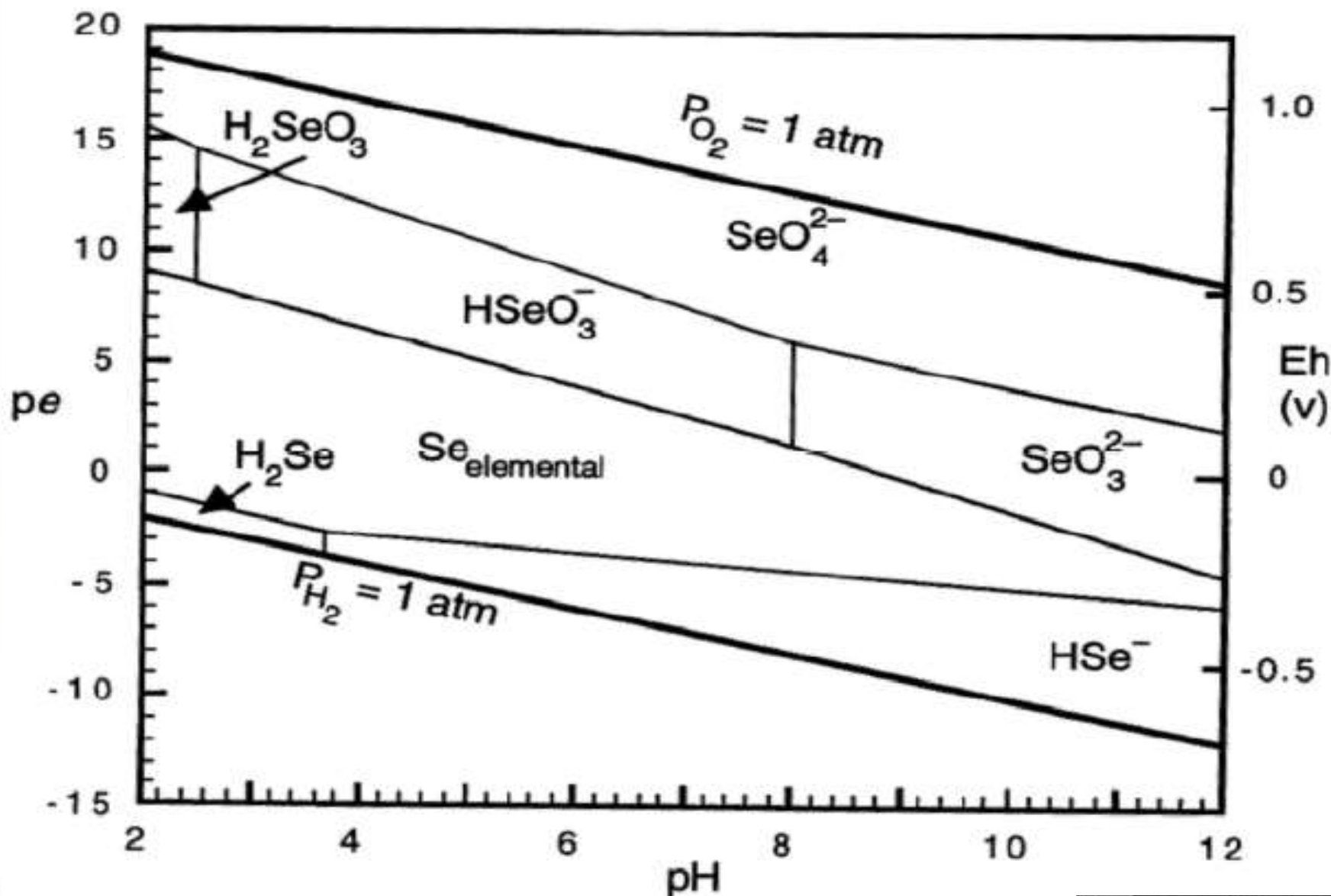
❖ Key System Details

- 2200 GPM pumping capacity via seven pumps
- Surface Runoff Selenium concentrations found to be low, during precipitation events
- Pump capacity nearly three times avg. flow, equivalent to 9.7 acre-ft./day
- Level Controlled Automatic pump operation
- 60 acre feet of storm water storage and flow equalization volume
- System Owning and Operating cost is estimated at \$0.38/1000 Gallons 10 yr. period, 8% NPV

Results of Focused Feasibility of Selected Technologies

| Treatment Technology | Estimated O&O Cost \$/1000 Gal. 10yr | Pro's | Con's |
|---------------------------------|---|--|---|
| Semi-Passive Biological Reactor | \$0.38 | Low Maintenance, No Residual Material Handling Issues, Self Sustaining, Low Cost Operation Have installed similar systems that have shown long term success | Large footprint required, initial startup equilibrium period, Reaction to higher Se concentration is time consuming |
| Ion Exchange | \$3.90 | Small Footprint required, Reaction period for higher Se Concentrations short. | Labor intensive, Residual Brine handling issue, Active mechanical maintenance issues. High Cost Operation, Treatment materials require storage, spill control |
| Zero Valent Iron | \$3.00-\$5.00 | Small Footprint required, Reaction period for higher Se Concentrations short. | Labor intensive, Residual Iron handling issue, Active mechanical maintenance issues. High Cost Operation, Treatment materials require storage, spill control Iron sludge handling and cost |

Chemistry of Selenium Treatment



Chemistry of Selenium Treatment

- ❖ Most Treatment Strategies (except Ion exchange & Reverse Osmosis) Reduce Selenate (+6) to Selenite (+4) Elemental (0) or Selenide (-2) form.
- ❖ Reducing Condition can be created either chemically or biologically.
- ❖ Chemically by a reducing agent (e.g., -ZVI), biologically through decomposing organic matter and/or microbial respiration processes

Chemistry of Selenium Treatment in Bio-Reactor

- ❖ $4\text{CH}_3\text{COO}^- + 3\text{SeO}_4^{2-} \rightarrow \text{Se}^0 + 8\text{CO}_2 + 4\text{H}_2\text{O} + 4\text{H}^+$
- ❖ Selenium (Selenate/Selenite) is reduced to its elemental state, where it precipitates out of solution and remains in the bio-reactor substrate.
- ❖ Key Factors to Removal
 - Form of Selenium, Arch-Eastern waters are > 95% Selenate
 - Eh (oxidation/Reduction) potential of the system
 - Affected by Temperature, Biological Activity, Flow Rate
 - Hydraulic Retention Time (detention time in the system)
 - Affected by Theoretical HRT (volume of the Bio-Reactor)
 - Affected by Actual HRT (Flow patterns within the system).

Demonstration Bio-reactor Results

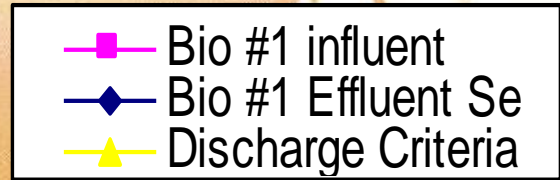
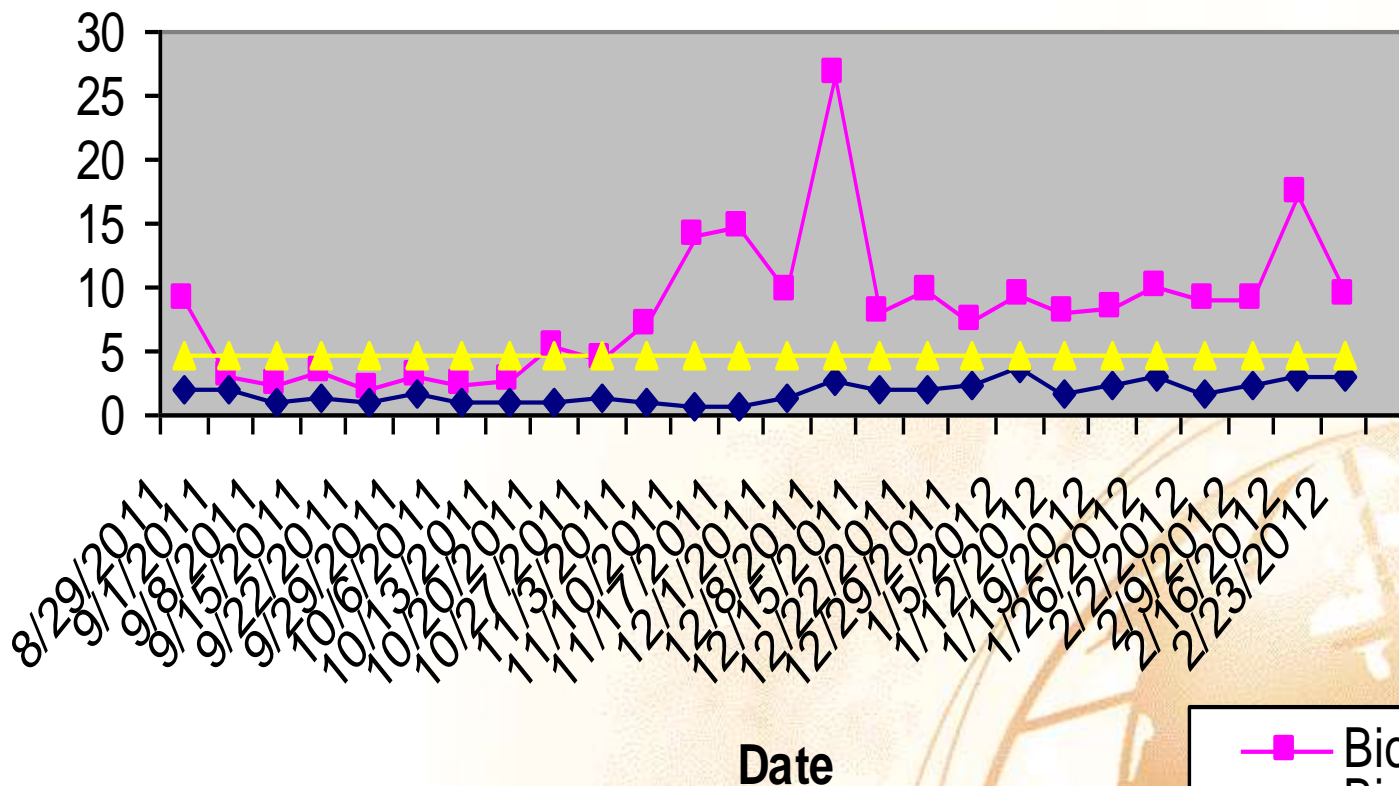






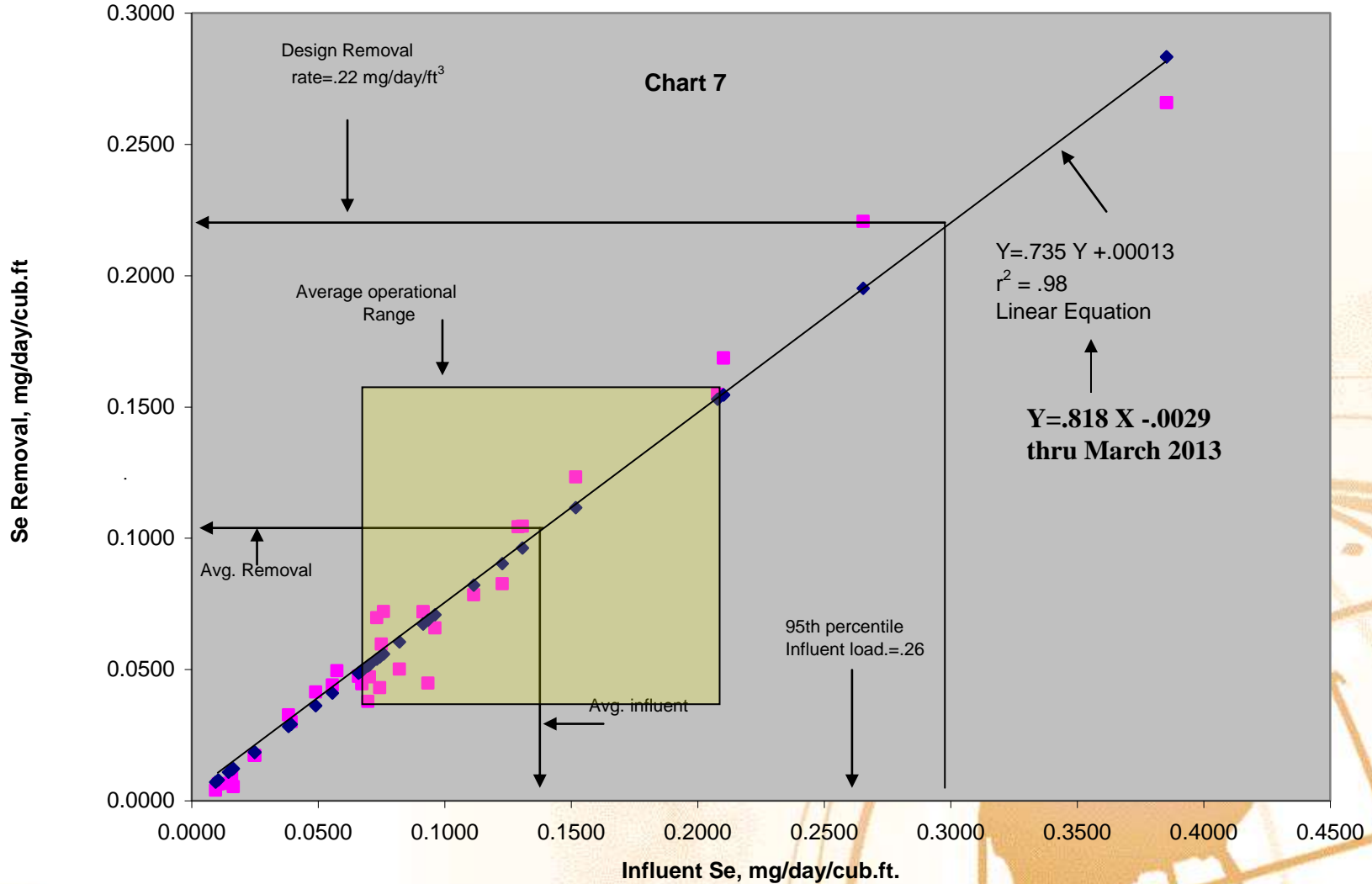
Arch-Eastern, Bioreactor # 1

Selenium Conc. (ug/l)



Arch-Eastern, Full Scale Bio-reactor
250,000 cubic foot, of Media
Design Se Removal Rate= .022 mg/day/ft³
2010 DMR and Modeled Flow rates

■ Data
 ◆ Linear Equation



Full Scale Implementation

- ❖ Full Scale Design Criteria (Established earlier in the project).
 - Flow 800 gpm
 - 95th Percentile Se concentration- 14.88
 - Effluent Concentration -2.35 µg/l (1/2 discharge criteria)
 - Yields a required Se removal of - 54635 mg Se/day
- ❖ Selenium removal rates of bio-reactor treatment established during demonstration testing
 - 0.22 mg/day/ft³
- ❖ Full Scale Bio-Reactor Size
 - $54635 \text{ mg/day} / .22 \text{ mg/day/ft}^3 = 248,340 \text{ ft}^3$

SYSTEM DESIGN





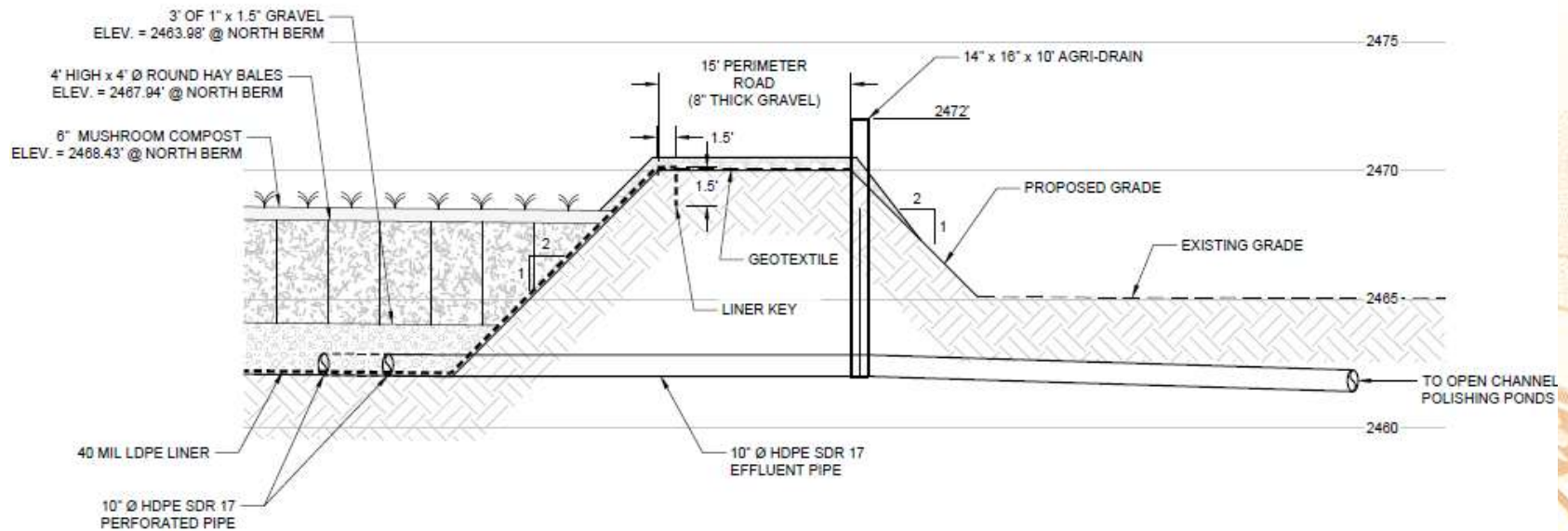








Full scale Bio-reactor Design, Outlet section



DETAIL 2 NORTH BERM CONSTRUCTION

HORIZ 1" = 10'
VERT 1" = 5'

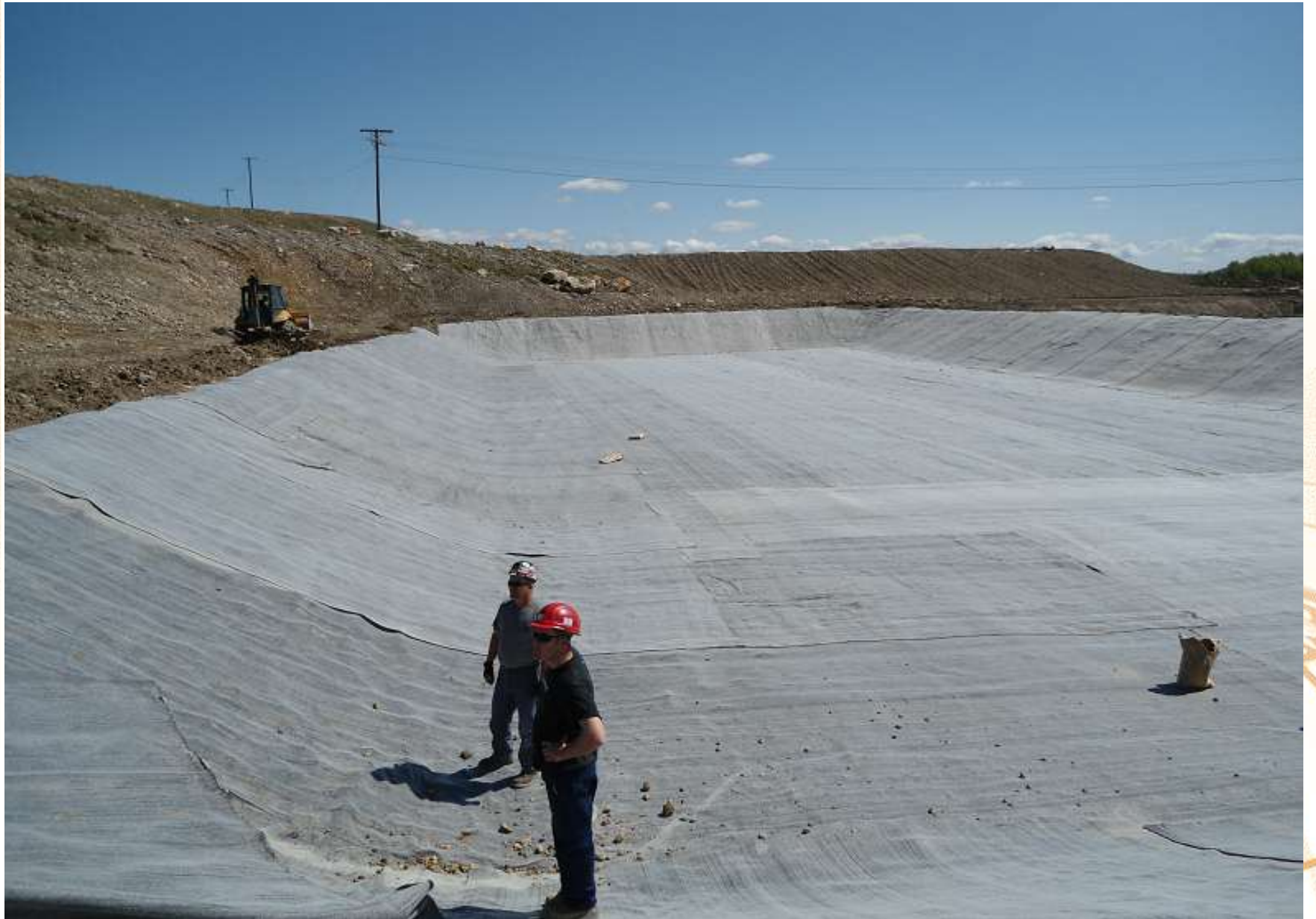
C-02

























System Cost

Construction Self Performed by Arch

❖ Estimated Cost

- Collection and Transfer System- \$1.8 Million
- Bioreactor Treatment System \$0.6 Million
- » Total \$2.4 Million

❖ Actual Cost

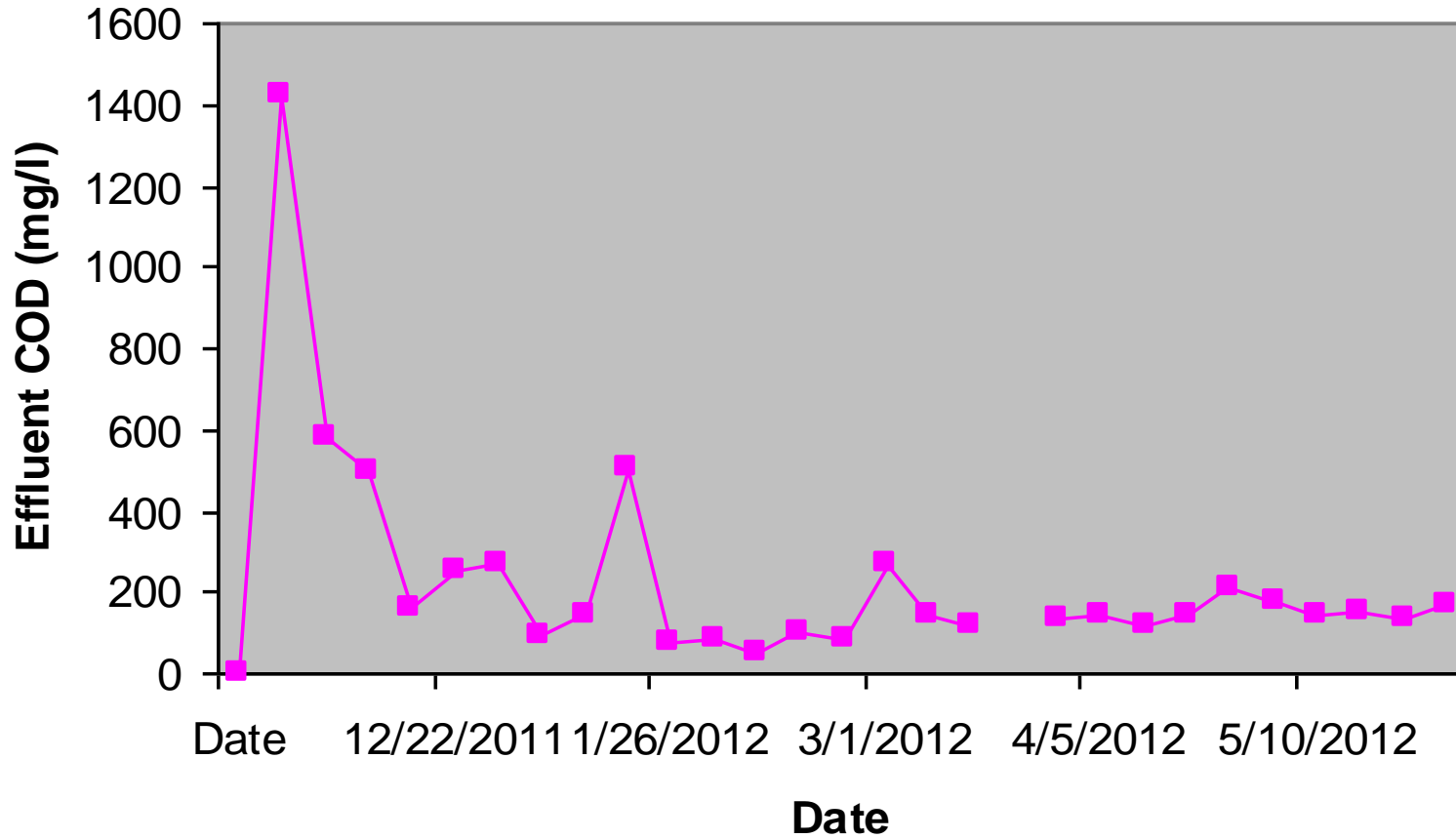
- Collection and Transfer System- \$1.6 Million
- Bioreactor Treatment System \$0.5 Million
- » Total \$2.1 Million

SYSTEM START UP

SYSTEM EQUILIBRIUM



Demonstration Bioreactor



Equilibrium Period, Full Scale System

| Date | Flow | COD mg/l PP 1 in | COD mg/l PP2 out | COD Rm lb/hr |
|-----------|------|---------------------|---------------------|-----------------|
| 6/1/2012 | 350 | 6610 | 4620 | 349 |
| 6/21/2102 | 459 | 292 | 39 | 58 |
| 6/28/2012 | 417 | 166 | 118 | 10 |
| 7/12/2012 | 1000 | 143 | 122 | 11 |
| 8/7/2012 | 938 | 136 | 42 | 44 |
| 8/14/2012 | 1000 | 125 | 41 | 42 |



System Performance

Modeled vs. Measured Flows

Hydrologic Modeling to Develop
Design Basis

Pump Hrs X Measured pump rate = Measured Flow

| Date | 001Pump Hr meter hrs | Day/period | Pump Rate gpm | Avg. Flow for period (gpm) | Pump Op. % of time | Rainfall inches | Rainfall per day (in) |
|------------|-------------------------|------------|------------------|-------------------------------|-----------------------|--------------------|--------------------------|
| 6/25/2012 | 51 | | 470 | | | | |
| 6/29/2012 | 68.3 | 4 | 470 | 85 | 18.02% | 0.98 | 0.25 |
| 7/19/2012 | 147 | 20 | 470 | 77 | 16.40% | 1.98 | 0.10 |
| 8/1/2012 | 340.1 | 13 | 470 | 291 | 61.89% | 6.24 | 0.48 |
| 8/8/2012 | 439.6 | 7 | 470 | 278 | 59.23% | 0.82 | 0.12 |
| 8/14/2012 | 537 | 6 | 470 | 318 | 67.64% | 1 | 0.17 |
| 8/21/2014 | 605.4 | 7 | 470 | 191 | 40.71% | 0.86 | 0.12 |
| 8/27/2012 | 614.7 | 6 | 470 | 30 | 6.46% | 0.4 | 0.07 |
| 9/4/2012 | 675.4 | 8 | 470 | 149 | 31.61% | 0.8 | 0.10 |
| 9/20/2012 | 825.6 | 16 | 470 | 184 | 39.11% | 2.67 | 0.17 |
| 10/8/2012 | 950.2 | 19 | 470 | 128 | 27.32% | 1.95 | 0.10 |
| 11/30/2102 | 1531.5 | 53 | 470 | 215 | 45.70% | 1.83 | 0.03 |
| 1/2/2013 | 2051.9 | 33 | 470 | 309 | 65.71% | 4.71 | 0.14 |

TOTAL FLOW 55,937,520
 Minutes/per. 264,960
 Gpm 211
 Avg Pump OP 39.98%

Modeled Flow vs. Measured Flow

| Pump ID. | 001 | 005 | 007 | 021 | 031 | 036 | Total (gpm) |
|--|--------------------------------|----------------------------------|--------|--------|--------|-------|---------------|
| Avg. Flow- 6 month period (<u>Modeled gpm</u>) | 164 | 108 | 128 | 91 | 100 | 43 | 635 |
| Avg. Flow - 6 month period (<u>Measured gpm</u>) | 211 | 121 | 181 | 82 | 73 | 37 | 705 |
| Flows Range Observed (gpm) | 30-318 | 5-329 | 36-441 | 14-223 | 30-154 | 1-115 | |
| Pump Utilization | 40% | 21% | 41% | 19% | 16% | 11% | |
| Measured/Modeled Flow Ratio | 1.29 | 1.11 | 1.41 | 0.90 | 0.73 | 0.87 | Ratio 1.11 |
| Measured/Modeled Precipitation Ratio | Modeled Precip. In. 22.9 | Measured Precip. In. 24.24 | | | | | Ratio 1.06 |

Selenium Treatment

SYSTEM PERFORMANCE

Summary to Date

- ❖ **No non-compliant discharges for Selenium since installation (9 months)**
- ❖ **Median Se Removal Rate = 81%**
- ❖ **Average Se Removal Rate = 72%**
- ❖ **Raw water Selenium concentrations ranged from 8.2 to 2.0 ug/l. Less than Design Concentrations**
- ❖ **Lowest Removal Rates observed during high flow that result in lower HRT and Higher ORP**

SYSTEM OPERATION



PUMP SYSTEM MONITOR PANEL



| Structure | Depth to Bottom of Weir (in) | Depth to top of water (FT) | Depth to top of water (in) | Flow CFS | Flow GPM | Total GPM | Internal H*1.5 | Head (FT) | C = See Reference above | L = Width Rect. Weir (FT) | ORP | Temp °C | Temp °F | EQ Basn pool el below Riser top (in) |
|-----------|------------------------------|----------------------------|----------------------------|----------|----------|-----------|----------------|-----------|-------------------------|---------------------------|------|---------|---------|--------------------------------------|
| AD-1 | 64.2 | 4.95 | 59.4 | 1.14 | 509.56 | | 0.25 | 0.40 | 4.47 | 1.083 | -184 | 6.9 | 44.42 | |
| AD-2 | 64.2 | 4.92 | 59.04 | 1.26 | 564.55 | 1074.1 | 0.28 | 0.43 | 4.47 | 1.083 | -172 | 7.4 | 45.32 | |
| PP2 weir | 8 | | 3.4375 | 2.38 | | 1068.3 | 0.23 | 0.38 | 3.33 | 3.125 | | | | -28 |
| AD-1 | 64.2 | 4.96 | 59.52 | 1.09 | 488.32 | | 0.24 | 0.39 | 4.45 | 1.083 | -184 | 6.9 | 44.42 | |
| AD-2 | 64.2 | 4.93 | 59.16 | 1.21 | 542.48 | 1030.8 | 0.27 | 0.42 | 4.45 | 1.083 | -172 | 7.4 | 45.32 | |
| PP2 weir | 8 | | 3.5625 | 2.28 | | 1025.4 | 0.22 | 0.37 | 3.33 | 3.125 | | | | -29 |
| AD-1 | 64.2 | 4.96 | 59.52 | 1.06 | 477.70 | | 0.24 | 0.39 | 4.35 | 1.083 | -183 | 6.7 | 44.06 | |
| AD-2 | 64.2 | 4.93 | 59.16 | 1.18 | 530.68 | 1008.4 | 0.27 | 0.42 | 4.35 | 1.083 | -175 | 6.5 | 43.7 | |
| PP2 weir | 8 | | 3.625 | 2.24 | | 1004.1 | 0.22 | 0.36 | 3.33 | 3.125 | | | | -29 |
| AD-1 | 64.2 | 5.08 | 60.96 | 0.67 | 298.74 | | 0.14 | 0.27 | 4.61 | 1.083 | -182 | 3 | 37.4 | |
| AD-2 | 64.2 | 5.11 | 61.32 | 0.56 | 251.82 | 550.6 | 0.12 | 0.24 | 4.61 | 1.083 | -182 | 4 | 39.2 | |
| PP2 weir | 8 | | 5.0625 | 1.24 | | 556.8 | 0.12 | 0.24 | 3.33 | 3.125 | | | | -42 |
| AD-1 | 59.2 | 4.65 | 55.8 | 0.74 | 330.24 | | 0.15 | 0.28 | 4.75 | 1.083 | -177 | 4.5 | 40.1 | |
| AD-2 | 59.2 | 4.7 | 56.4 | 0.56 | 249.21 | 579.4 | 0.11 | 0.23 | 4.75 | 1.083 | -186 | 4.2 | 39.56 | |
| PP2 weir | 8 | | 4.9375 | 1.32 | | 592.3 | 0.13 | 0.26 | 3.33 | 3.125 | | | | -42 |
| AD-1 | 59.2 | 4.7 | 56.4 | 0.72 | 324.16 | | 0.11 | 0.23 | 6.18 | 1.083 | -194 | 2.6 | 36.68 | |
| AD-2 | 59.2 | 4.76 | 57.12 | 0.47 | 209.95 | 534.1 | 0.07 | 0.17 | 6.18 | 1.083 | -192 | 2 | 35.6 | |
| PP2 weir | 8 | | 5 | 1.28 | | 574.4 | 0.13 | 0.25 | 3.33 | 3.125 | | | | -43 |
| AD-1 | 59.2 | 4.63 | 55.56 | 0.84 | 377.19 | | 0.17 | 0.30 | 4.92 | 1.083 | -181 | 4.7 | 40.46 | |
| AD-2 | 59.2 | 4.68 | 56.16 | 0.65 | 290.70 | 667.9 | 0.13 | 0.25 | 4.92 | 1.083 | -179 | 4.5 | 40.1 | |
| PP2 weir | 8 | | 4.625 | 1.52 | | 684.1 | 0.15 | 0.28 | 3.33 | 3.125 | | | | -40 |
| AD-1 | 59.2 | 4.72 | 56.64 | 0.33 | 147.12 | | 0.10 | 0.21 | 3.20 | 1.083 | -178 | 6.2 | 43.16 | |
| AD-2 | 59.2 | 4.75 | 57 | 0.26 | 117.88 | 265.0 | 0.08 | 0.18 | 3.20 | 1.083 | -189 | 5.8 | 42.44 | |
| PP2 weir | 8 | | 6.25 | 0.57 | | 257.7 | 0.06 | 0.15 | 3.33 | 3.125 | | | | -46 |
| AD-1 | 47.2 | 3.68 | 44.16 | 0.41 | 183.33 | | 0.13 | 0.25 | 3.10 | 1.083 | -201 | 8.6 | 47.48 | |
| AD-2 | 47.2 | 3.72 | 44.64 | 0.32 | 142.77 | 326.1 | 0.10 | 0.21 | 3.10 | 1.083 | -225 | 7.7 | 45.86 | |
| PP2 weir | 8 | | 6 | 0.70 | | 314.4 | 0.07 | 0.17 | 3.33 | 3.125 | | | | -42 |
| AD-1 | 52.2 | 4.12 | 49.44 | 0.49 | 221.94 | | 0.11 | 0.23 | 4.32 | 1.083 | -196 | 6.2 | 43.16 | |
| AD-2 | 52.2 | 4.15 | 49.8 | 0.40 | 181.01 | 402.9 | 0.09 | 0.20 | 4.32 | 1.083 | -221 | 8.1 | 46.58 | |
| PP2 weir | 8 | | 5.625 | 0.90 | | 406.0 | 0.09 | 0.20 | 3.33 | 3.125 | | | | -46 |

OPERATIONAL LESSONS LEARNED

- ❖ ORP is the best indicator of operational performance
 - Flow rate and Temp. affect ORP
 - ORP and Hyd. Retention time affect selenium removal rates
- ❖ System Start-up (Eq. period) can be a challenge
 - Ambient Temp affect COD level
 - Flow Rate affect COD level
- ❖ Consolidation of discharges (collection & transfer) has had un-anticipated benefits.
 - Less monitoring labor
 - Has allowed for more economical treatment reagents for manganese control that will save significant \$'s in treatment costs.

Longevity of System?

- ❖ Good Question!!
- ❖ Hay is the Carbon source, and Carbon is used up in the treatment process.
- ❖ Demonstration Bioreactor lost 25% of hay volume in 1 yr of operation.
- ❖ Some hay loss do to compaction and settling
- ❖ Cattail production can supplement hay loss
- ❖ Bioreactors of this type, will require supplemental hay addition on a periodic basis